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# A NOVEL TIMBER DOWEL-TYPE CONNECTION USING SHAPE MEMORY ALLOY

Haoyu Huang<sup>1</sup>, Wen-Shao Chang<sup>2</sup>

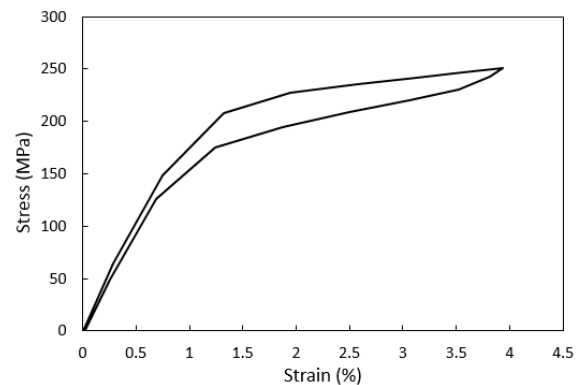
**ABSTRACT:** In order to provide self-centering effect, a novel timber dowel-type connection system using superelastic shape memory alloy (SMA) bar and tubes as dowels is investigated in this study. Double-shear connections with SMA and mild steel dowels were tested under dynamic loadings at different displacement levels. The results showed that SMA dowel-type connections have good self-centering behaviours and can mitigate the residual deformation effectively compared with steel dowel-type connections after excessive deformation, although the steel dowel-type connections present higher strength. These tests reveal that the connection with tube dowels show higher equivalent viscous damping ratio than those use solid bar as tube would allow larger deformation to dissipate energy.

**KEYWORDS:** Timber dowel-type connection, Shape memory alloy; Tubes; Self-centering effect

## 1 INTRODUCTION

In timber structures, connection is an important component because the connection is the weakest link of a structure. The stiffness of the connections significantly affects the structural deformation behaviours [1]. Concerning the conditions under cyclic loading, damping capacity of connections plays an important role in energy dissipation. Dowel-type connection is the most common type of timber connection, mainly relying on the bending capacity of the dowel and the embedment of the timber [2].

Nevertheless, timber connections are always the weakest in the whole structure under an extreme event such as an earthquake. Steel is normally used in dowel-type connections, because steel contributes satisfactory stiffness and strength and has the benefit of low cost. However, as presented in our pilot studies [3], steel dowels in timber connections have large residual deformations, and residual deformations from connections can cause structural instability and collapse, so it is important to develop a self-centering connection system. Therefore, we used a dowel-type connection using superelastic shape memory alloy (SMA) dowel in our pilot research [3] and preliminary static compressive tests showed it was capable of being self-centering.



**Figure 1:** Stress-strain curve of Cu-Al-Mn SMA bar tensile test

Superelasticity is one of the most important characteristics of SMA [4]. Figure 1 presents the result from one of our previous tensile tests on Cu-Al-Mn (Cu = 81.84%, Al = 7.43% and Mn = 10.73% by weight) SMA bars, and shows the superelastic behaviour which is able to recover the alloy to the original shape after a large plastic deformation. The application of SMA to civil engineering has been explored in previous research and the mechanical characteristics of SMA have been studied in relation to its performances in structures [5-12]. The fatigue properties of copper-based SMA have been studied regarding to its structural applications, and the dependency on temperature and strain range is highlighted [13-15]. SMA has been studied in steel connections for reinforcement, and research results show SMA is able to recover residual deformations and exhibit satisfactory energy dissipation capacities [16-20]. With regard to the particular self-centering effect of SMA on

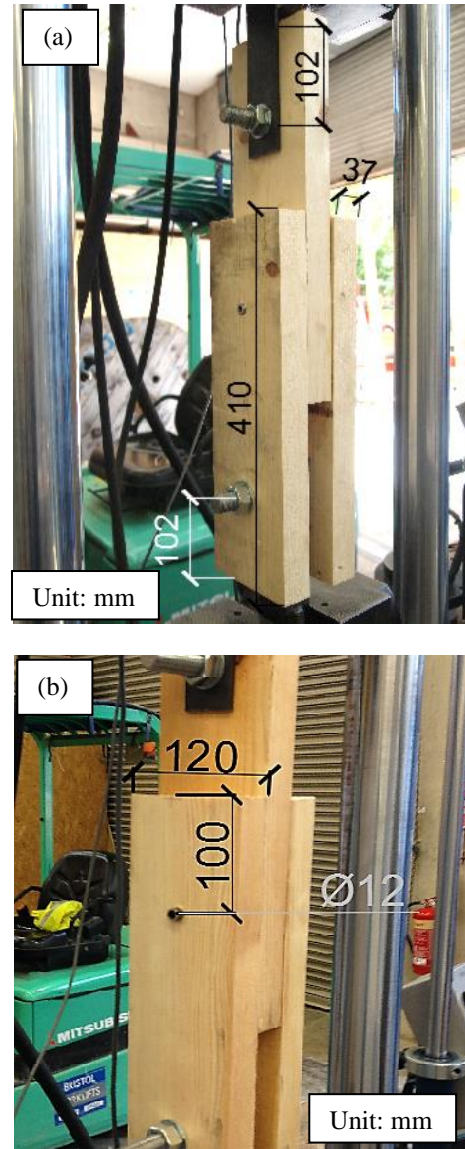
timber connections and the interest in whether SMA can benefit dowel-type timber connections, only our pilot research [3] has been carried out and more explorations are needed.

Associated with the enhancement of damping capacity for timber connections, Leijten [21] forwarded a concept that the solid dowel can be replaced by tube. Tube is easier to bend than a solid bar, thus the larger bending deformation can contribute more damping capacity [22]. Moreover, tube can be expanded by hydraulic jack in order to achieve suitable clearance with timber and in this way the stiffness of connection can be increased. However, the residual deformation of tubes caused by larger bending is an issue. The application of SMA tubes to timber connections would be practicable in addressing this problem.

In this study, a novel timber dowel-type connection with SMA is developed in which SMA solid bars and tubes are used as dowels to present self-recoverable function. Dynamic cyclic loadings with different amplitudes were carried out. Mild steel was employed in the same tests for comparison. This study presents how this novel dowel-type connection behaved in terms of self-centering capacity, damping ratio, strength and ductility. More resilience may lead to less energy dissipation because the unloading curve retrieves to the origin and the hysteresis loop becomes small, and this can be seen in the tests on SMA-reinforced beam-column joints [23]. To find the balance between energy dissipation and resilience in timber connections, a parametric study was carried out by analysing the effect of connections on seismic performance of a timber structure so as to provide a basic understanding.

## 2 MATERIALS AND METHODS

The dowel-type connection used in this study is a double-shear connection with three pieces of timber and one dowel. A total of 30 connections were tested in this project. The timber used in the fabrication is sawn softwood graded C24, and the species is spruce (*picea abies*). The embedment strength, moisture content and density were tested in the laboratory. The tests for embedment strength strictly followed the BS EN383 [24], and the characteristic embedment strength paralleled to grain was 18.95 MPa from 10 samples. The average moisture content and characteristic density were 11.3% and 306.78 kg/m<sup>3</sup>, respectively.



**Figure 2:** (a) Test setup of double-shear dowel-type timber connection; (b) Application of tube-type dowel to timber connection

The fastener connecting the timber used both SMA and steel tubes and bars with outer diameter of 12 mm. Cu-Al-Mn (Cu = 81.84%, Al = 7.43% and Mn = 10.73% by weight) SMA was employed in this study, and was provided by Furukawa Techno Material Co. Ltd., Japan. The material cost of copper-based SMAs is 10%-20% of that of Ni-Ti-based SMAs [6], and cost of Cu-Al-Mn SMA is as low as that of other copper-based SMAs [10]. Moreover, in comparison of Ni-Ti SMA, machining Cu-Al-Mn SMA is easy, thus the machining cost can be lower [10]. The austenitic phase transformation end temperature ( $A_f$ ) tested by the differential scanning calorimetry (DSC) method was -53°C, which means this Cu-Al-Mn SMA is superelastic at ambient temperature and has the aforementioned re-centering capacity. From material characterisation of Cu-Al-Mn SMA bars of 12 mm in diameter, the phase transformation stress was 200 MPa. The transformation stress of SMA has the dependence on temperature, e.g. the transformation stress increases with the rising temperature [25, 26]. The

material for steel dowel was mild steel graded EN3B (080A15) [27], and its yield stress was 310 MPa. To present the effect of tube-shape dowels on the dynamic behaviours of the connection, despite using solid rods, SMA and mild steel tubes with 6 mm and 8 mm inner diameter holes and 12 mm outer diameter were applied to the tests.

The dimensions of experimental connections and test setup can be seen in Figure 2. As listed in the test protocol (Table 1), comparison tests in terms of different dimensions and materials of dowels were carried out. For each test, the loading protocol can be seen in Figure 3; connection samples were tested by displacement control at displacement amplitudes of 2, 4, 6, 8, 10 and 12 mm at a loading frequency of 1 Hz. As the damping stabilisation issue of SMA has been discussed [28], the damping decaying of SMA dowel-type connections at invariant displacement is studied in this paper. Therefore, there are 10 cycles in each loading displacement level as shown in Figure 3. Each testing condition was repeated using 5 samples.

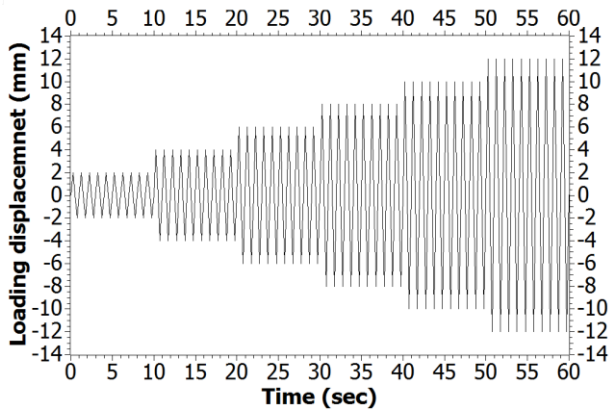


Figure 3: Loading protocol

Table 1: Test protocol

| Number of test | Material of the dowel | Dowel dimensions: diameter of the hole (mm) | Repetition number |
|----------------|-----------------------|---|-------------------|
| 1              | Cu-Al-Mn SMA          | 0 (Solid bar)                               | 5                 |
| 2              |                       | 6   | 5                 |
| 3              |                       | 8   | 5                 |
| 4              | Mild steel            | 0 (Solid bar)                               | 5                 |
| 5              |                       | 6   | 5                 |
| 6              |                       | 8   | 5                 |

### 3 RESULTS AND DISCUSSION

#### 3.1 FAILURE MODE

Figure 4 shows the observations of failure modes. As seen in Figure 4 (a) and (c), which present the transections of connections using steel bars and steel tubes with 6 mm diameter hole, the inner timber meets bearing failure and the hole area of that has an elongation of approximately dowel diameter length. Timber splitting failures are also observed in these two

types of connections, and were initiated by the embedment failure of the hole area. For connections using steel tubes and SMA dowels, as shown in Figure 4 (b), (c), (d), (e) and (f), the dowels are bent plastically and one plastic hinge occurs in the middle. SMA dowels and steel tubes have lower bending strength and, therefore, bend more easily. As a consequence, the inner timber embedment failures in these samples were smaller. It is noteworthy that steel tubes with 6 and 8 mm diameter hole and SMA tubes with 8 mm diameter hole were fractured after loading, as thin wall thickness leads to more bending deformation and low-cycle fatigue occurs. In Table 2, the deformations at which each type of connection fails are indicated. It can be found connections with steel receive more damage. For a stronger timber, the embedment failure of timber can be reduced, thus densified veneer wood will be considered to be employed in reinforcing timber connection in further research. Considering dowels with different diameter applied to the connections, the failure mode could be different and Johansen's equations can be referred. In this study, the effect of SMA tubes on failure mode is mainly studied and compared.

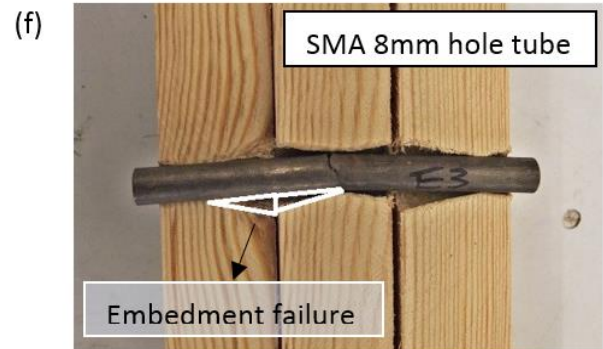
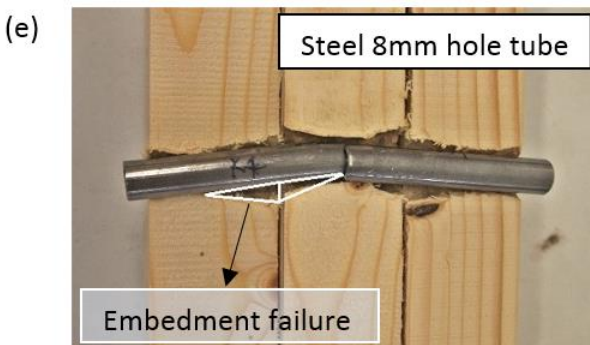
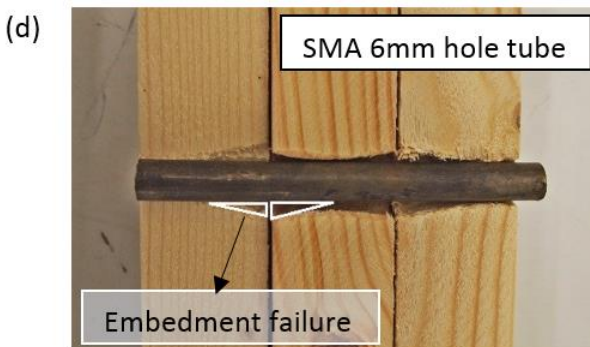
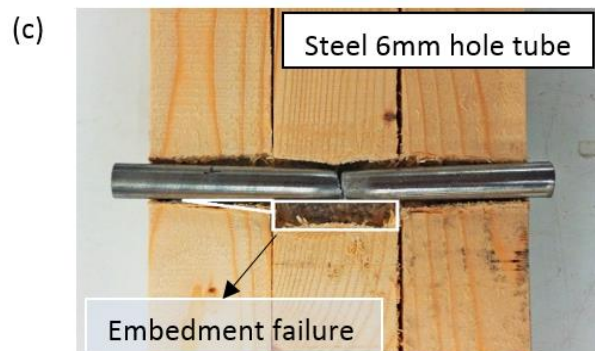
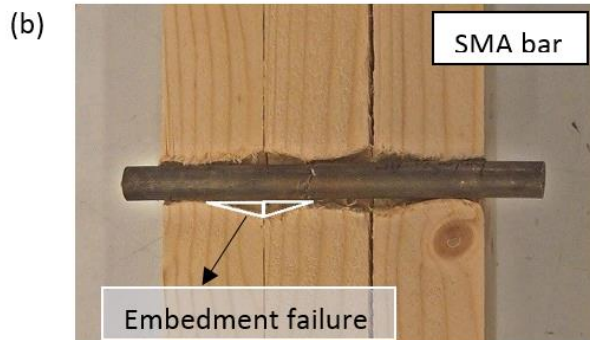
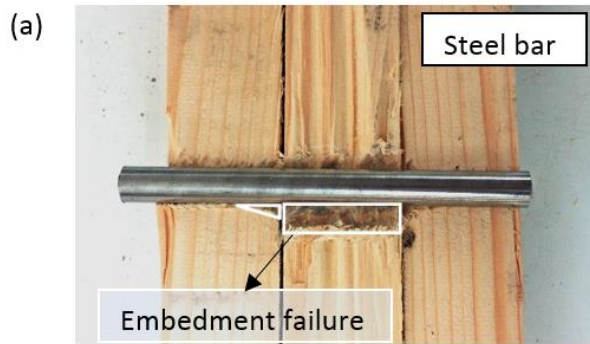
#### 3.2 SELF-CENTERING BEHAVIOURS

Load-displacement curves of timber dowel-type connections using mild steel and SMA bars and tubes are presented in Figure 5 and Figure 6, respectively. These two Figures show the last cycle (10<sup>th</sup> cycle) in each amplitude level. As the connection using a steel bar was broken at 10 mm amplitude, hysteresis at 10 mm and 12 mm amplitude of that does not show in Figure 5. In Figure 6, steel dowel-type connections were broken at 12 mm amplitude. Therefore, SMA allows larger deformation. From Figure 5 and 6, the residual displacement of SMA dowel-type connections is much smaller than that using mild steel. The timber SMA dowel-type connection shows good self-centering effect. The permanent deformation of SMA dowel-type connections is mainly contributed by timber embedment failure. In further studies, the self-centering effect of SMA dowels is expected to be more significant by reinforcing timber in order to increase the embedment strength.

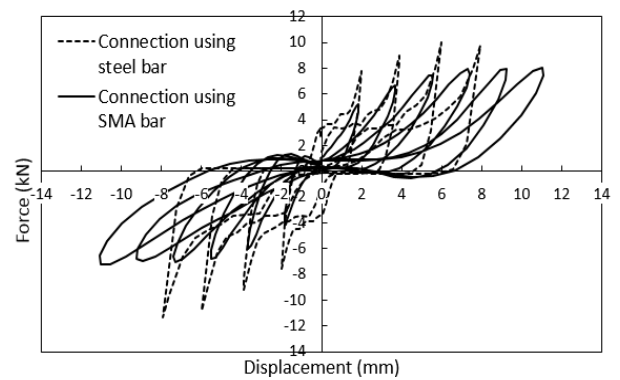
Table 2: Failing deformation of each type of connection

| Number of test | Material of the dowel | Dowel dimensions: diameter of the hole (mm) | Failing deformation (mm) |
|----------------|-----------------------|---|--------------------------|
| 1              | Cu-Al-Mn SMA          | 0 (Solid bar)                               | Did not fail             |
| 2              |                       | 6   | Did not fail             |
| 3              |                       | 8   |                          |
| 4              | Mild steel            | 0 (Solid bar)                               | 10                       |
| 5              |                       | 6   | 12                       |
| 6              |                       | 8   | 8                        |

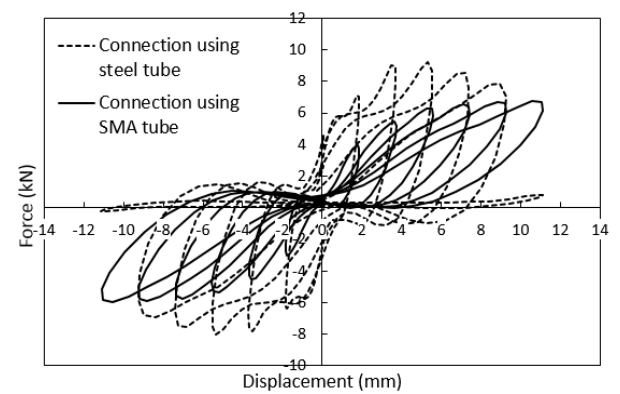




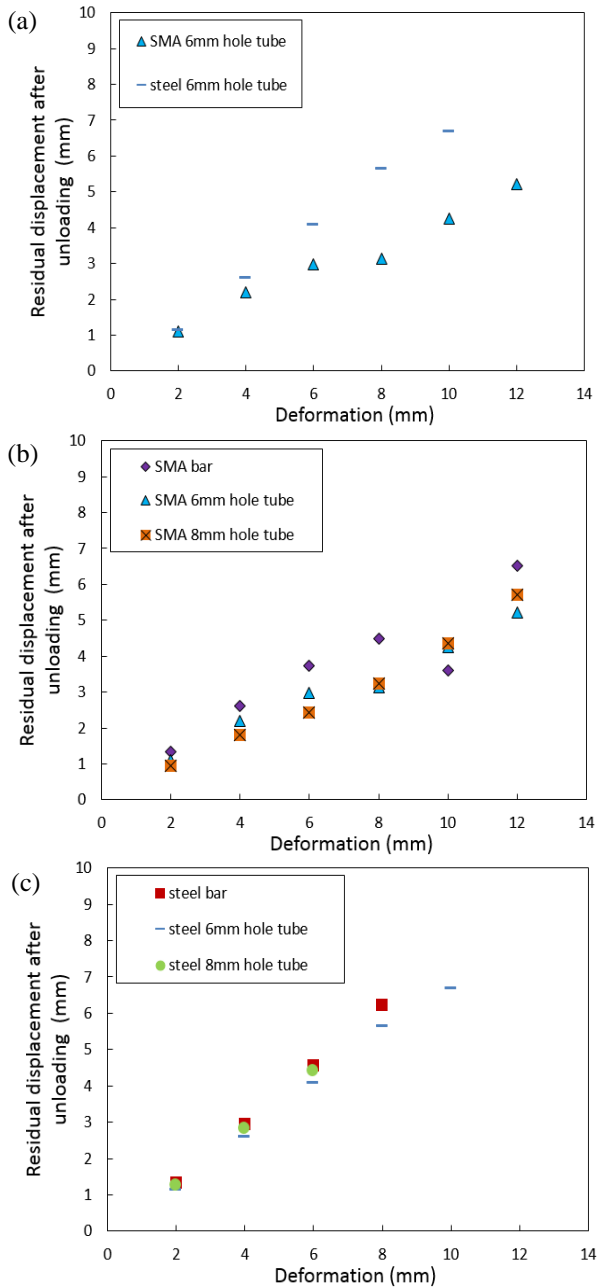
**Figure 4:** Failure modes for timber connections using (a) steel bar; (b) SMA bar; (c) steel tube with 6 mm diameter hole; (d) SMA tube with 6 mm diameter hole; (e) steel tube with 8 mm diameter hole; (f) SMA tube with 8 mm diameter hole



**Figure 5:** Load-displacement curve of timber dowel-type connections using steel and SMA bar (10th cycle)



**Figure 6:** Load-displacement curve of timber dowel-type connections steel and SMA tube (6 mm diameter hole) (10th cycle)



**Figure 7:** (a) Comparison of the residual displacement of the steel and SMA tube with 6mm hole dowel-type connection at 10th cycle at each amplitude level; (b) Residual displacement of the SMA dowel-type connections at 10th cycle at each amplitude level; (c) Residual displacement of the steel dowel-type connections at 10th cycle at each amplitude level

Figure 7 presents the residual deformation in the last cycle at each amplitude level. Since some steel dowel-type connections were broken before completing the loading protocol, in higher displacement levels, residual displacements of these do not show in the graph. In Figure 7 (a), the larger the loading amplitude, the better the self-centering behaviour of SMA dowel-type connections compared with steel dowel-type connections. For instance, at amplitude of 2 mm, the re-centering effect is not obvious, whilst the retrieval is large at amplitude of 10 mm. In SMA bar system as seen in Figure 7 (b), the residual displacement at 10 mm

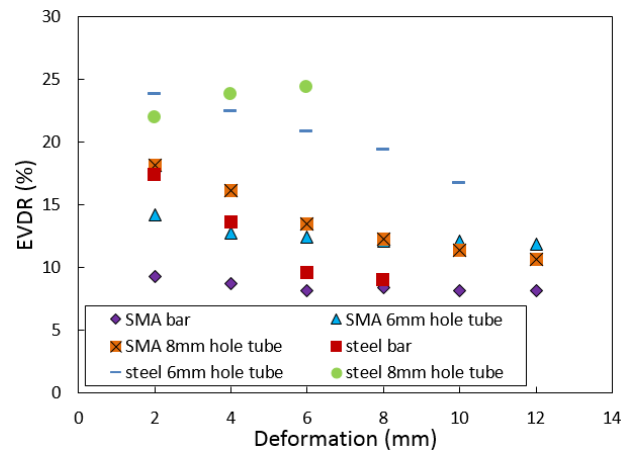
deformation is lower than that at 8 mm deformation; the behaviour could be caused by the self-heating of SMA as higher temperature can facilitate its superelasticity.

In SMA dowel-type connections, using tubes shows better self-centering effect, while this trend is weak in steel dowel-type connections in comparison of Figure 7 (b) and (c). It is of importance that the self-centering effect of SMA can be developed so as to mitigate the damage of connections and reduce the permanent deformation after earthquakes.

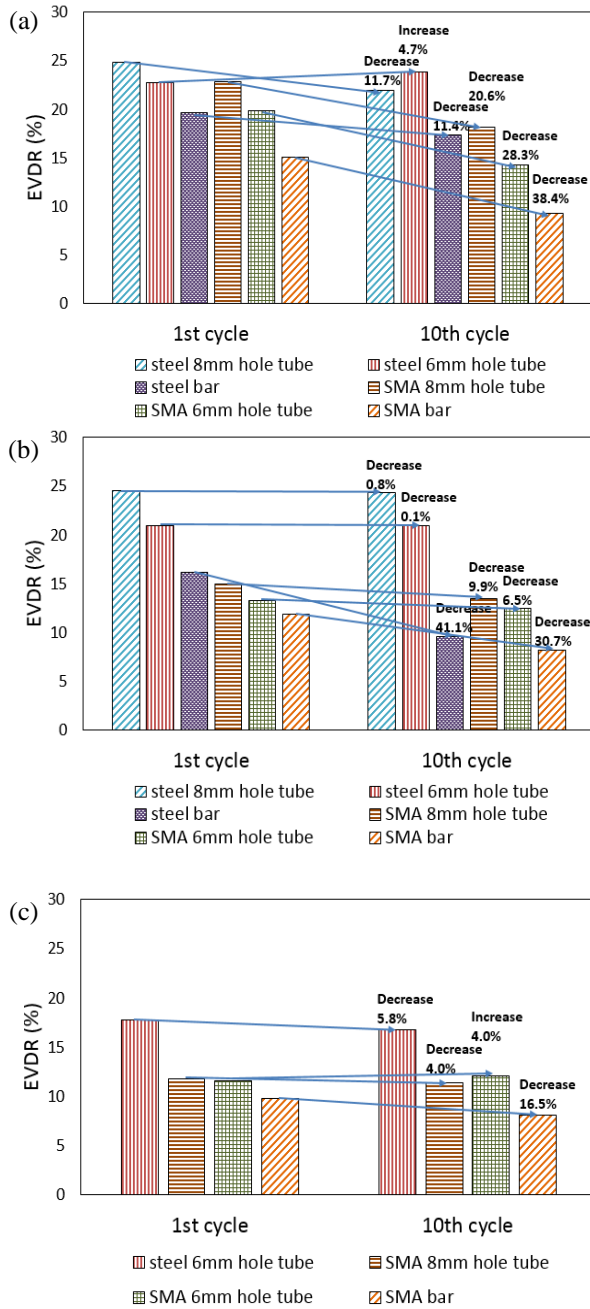
### 3.3 DAMPING PROPERTIES

Damping capacity of connections plays an important role in timber structures to dissipate energy. Equivalent viscous damping ratio (EVDR) of connections in each cycle is calculated based on the methods in BS EN12512 [29]. Comparing EVDR between steel dowels and SMA dowels in Figure 8, steel dowels contribute higher damping and the hysteresis of steel dowel-type connections covers larger area, as seen in Figure 5 and 6. Except for connections using steel tube with 8 mm diameter hole, EVDR decreases with the increase in loading amplitude.

It is noteworthy that tubes can increase the damping capacity of connections and the larger the hole, the more energy it can dissipate. It can be explained by the fact that tubes are easier to bend plastically and plastic hinges can increase the energy dissipation, as indicated in the Introduction. By converting SMA bars to tubes, the energy dissipation capacity can be comparable with that of a steel bar.



**Figure 8:** EVDR of the SMA and steel dowel-type connections at 10th cycle in each condition



**Figure 9:** Comparison of the EVDR of the timber dowel-type connection between 1st cycle and 10th cycle (a) at amplitude of 2 mm; (b) at amplitude of 6 mm and (c) at amplitude of 10 mm

Figure 9 (a), (b) and (c) compares the EVDR in the 1<sup>st</sup> cycle and 10<sup>th</sup> cycle at amplitude of 2 mm, 6 mm and 10 mm, respectively. The variable proportions are presented on each graph. Figure 9 (a) shows how energy dissipation drops down from the 1<sup>st</sup> cycle to the 10<sup>th</sup> cycle and the decrement of SMA dowel-type-connections is greater than that of steel. In the first cycle, the damping capacity of timber connections depends on both dowel and timber deformation. After the first cycle, timber often meets bearing failure and only dowel dissipates energy and that is why damping decreases. The larger damping decay in SMA dowel-type connections is caused by microstructural dislocation and slip. The internal stress of SMA contributed by microstructural deformation can facilitate the formation

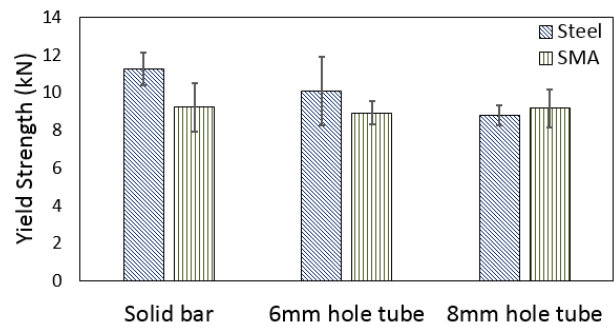
of martensite, which results in the drop of critical yield stress; in the consequence it leads to less energy dissipation [9, 30]. However, this damping decrement tends to be small when the dislocation stabilises, and this phenomenon can be seen in Figure 9 (b) and 9 (c). Figure 9 (b) compares EVDR in the further loading at amplitude of 6 mm; the decrement of damping of SMA dowels tends to be smaller after 10 cycles, whilst the EVDR of steel bar connections decreases greatly and may be due to low-cycle fatigue. In the following loading procedures, as shown in Figure 9 (c), SMA shows little damping decay between the 1<sup>st</sup> and 10<sup>th</sup> cycle, while connections using steel bars and steel tubes with 8 mm hole are broken. It is notable EVDR compared in study is regarded as from a whole connection even though the damage of the wood is different in each series.

### 3.4 STRENGTH AND DUCTILITY

The yield strength of connections is calculated using the approach in BS EN12512 [29] and is shown in Figure 10. Ultimate strength is presented in Figure 11. These values are averaged from 5 repetitions and the error bars show the standard deviation. It can be seen that steel dowels can provide higher strength for 1-2 kN than SMA dowels, except in the condition using 8 mm diameter hole tubes. The yield strength of SMA dowel-type connections is not influenced so much by converting solid bars to tubes, while the yield strength of steel dowel-type connections is reduced by using tubes. The ductility is calculated by the formula based on BS EN12512 [29]:

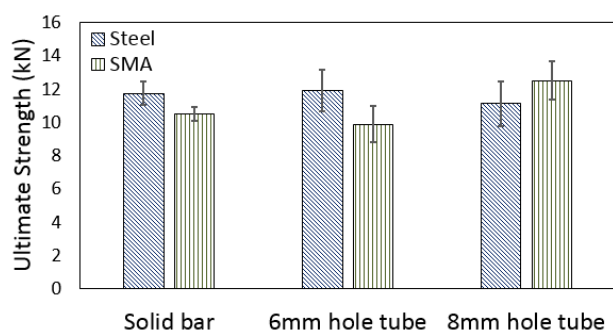
$$D = \frac{V_u}{V_y}$$

where  $V_u$  is the ultimate slip and  $V_y$  is the yield slip. Figure 12 shows the averaged ductility ( $D$ ) using 5 samples. The ductility of connection using solid SMA bars is the highest. The reason is that steel was fractured before completing the loading protocol and SMA allows larger deformation, as seen in Figure 5. In terms of steel dowels, 6 mm diameter tubes provide higher ductility. As shown in Figure 6, the elastic stiffness of SMA tube dowel-type connections is lower and leads to lower ductility.

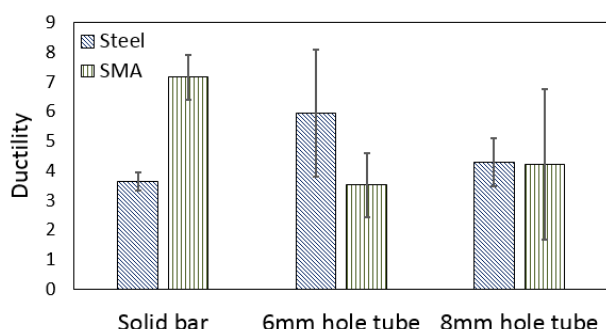


**Figure 10:** Yield strength of steel and SMA timber dowel-type connections





**Figure 11:** Ultimate strength of steel and SMA timber dowel-type connections



**Figure 12:** Ductility of steel and SMA timber dowel-type connections

## 4 CONCLUSION

In this study, novel timber connections using SMA solid bars and SMA tubes as dowels are investigated. With regard to performance under earthquake, the connections were tested under dynamic cyclic loadings at between 2 and 12 mm amplitudes. SMA dowel-type connections show good self-centering effect compared with steel dowel-type connections and can effectively reduce residual deformation, especially at a larger displacement level in which SMA tubes present better self-centering properties. Timber connections with steel have more damping than with SMA, however, receive more damage. The energy dissipation capacity of SMA dowel-type connections is found to be improved by applying thinner-wall-thickness tubes. The equivalent viscous damping ratio decay in the first cycles is observed both in steel and SMA. Decrement in SMA is more, but tends to stabilise. The strength of steel dowel-type connections is relatively higher except in the condition using 8 mm diameter hole tubes. It is noteworthy that the application of SMA tubes to timber connections shows better self-centering effect, higher damping and comparable strength with steel.

## ACKNOWLEDGEMENT

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## REFERENCES

- [1] Porteous J, Kermani A. Structural timber design to Eurocode 5. 2nd edition ed. Chichester: Wiley-Blackwell; 2013.
- [2] Thelandersson S, Larsen HJ. Timber engineering. Chichester: Wiley; 2003.
- [3] Chang WS, Murakami S, Komatsu K, Araki Y, Shrestha K, Omori T et al. Technical Note: Potential to Use Shape Memory Alloy in Timber Dowel-Type Connections. Wood Fiber Sci. 2013;45:330-4.
- [4] Duerig TW. Engineering aspects of shape memory alloys. London ; Boston: Butterworth-Heinemann; 1990.
- [5] Ozbulut OE, Hurlebaus S, Desroches R. Seismic response control using shape memory alloys: a review. J Intel Mat Syst Str. 2011;22:1531-49.
- [6] Janke L, Czaderski C, Motavalli M, Ruth J. Applications of shape memory alloys in civil engineering structures - Overview, limits and new ideas. Mater Struct. 2005;38:578-92.
- [7] Desroches R, Smith B. Shape memory alloys in seismic resistant design and retrofit: A critical review of their potential and limitations. Journal of earthquake engineering. 2004;8:415-29.
- [8] Dolce M, Cardone D. Mechanical behaviour of shape memory alloys for seismic applications - 2. Austenite NiTi wires subjected to tension. Int J Mech Sci. 2001;43:2657-77.
- [9] DesRoches R, McCormick J, Delemont M. Cyclic properties of superelastic shape memory alloy wires and bars. J Struct Eng-Asce. 2004;130:38-46.
- [10] Araki Y, Endo T, Omori T, Sutou Y, Koetaka Y, Kainuma R et al. Potential of superelastic Cu-Al-Mn alloy bars for seismic applications. Earthquake Eng Struc. 2011;40:107-15.
- [11] Huang H, Chang W-S. Feasibility of shape memory alloy in a tuneable mass damper to reduce excessive in-service vibration. Structural Control and Health Monitoring. 2016.
- [12] Huang H, Xie W, Chang W-S. Materials Characterization of NiTi and CuAlMn Shape Memory Alloy Bars under Dynamic Bending. SMST 2015: The Model for Shape Memory Application, Proceedings of the Shape Memory and Superelastic Technologies Conference. Chipping Norton, Oxfordshire, UK2015.
- [13] Casciati S, Marzi A. Experimental studies on the fatigue life of shape memory alloy bars. Smart Struct Syst. 2010;6:73-85.
- [14] Casciati S, Marzi A. Fatigue tests on SMA bars in span control. Engineering Structures. 2011;33:1232-9.
- [15] Carreras G, Casciati F, Casciati S, Isalgue A, Marzi A, Torra V. Fatigue laboratory tests toward the design of SMA portico-braces. Smart Struct Syst. 2011;7:41-57.
- [16] Speicher MS, DesRoches R, Leon RT. Experimental results of a NiTi shape memory alloy (SMA)-based recentering beam-column connection. Engineering Structures. 2011;33:2448-57.
- [17] Guo B, Gu Q, Liu F. Experimental behavior of stiffened and unstiffened end-plate connections under cyclic loading. J Struct Eng-Asce. 2006;132:1352-7.
- [18] Ma HW, Wilkinson T, Cho CD. Feasibility study on a self-centering beam-to-column connection by using the



superelastic behavior of SMAs. *Smart Mater Struct.* 2007;16:1555-63.

[19] Sepulveda J, Boroschek R, Herrera R, Moroni O, Sarrazin M. Steel beam-column connection using copper-based shape memory alloy dampers. *J Constr Steel Res.* 2008;64:429-35.

[20] Moradi S, Alam MS. Feasibility study of utilizing superelastic shape memory alloy plates in steel beam-column connections for improved seismic performance. *J Intel Mat Syst Str.* 2015;26:463-75.

[21] Leijten AJM. Development of reinforced joints with densified veneer wood. *Proc, 1991 Int Timber Engineering Conf* 1991. p. 36-42.

[22] Leijten AJM, Ruxton S, Prion H, Lam F. A novel timber connection with exceptional properties 13th World Conference on Earthquake Engineering. Vancouver, B.C., Canada 2004.

[23] Youssef MA, Alam MS, Nehdi M. Experimental investigation on the seismic behavior of beam-column joints reinforced with Superelastic Shape Memory Alloys. *Journal of Earthquake Engineering.* 2008;12:1205-22.

[24] British Standards Institution. BS EN 383:2007 - Timber structures - Test methods - Determination of embedment strength and foundation values for dowel type fasteners: BSI; 2007.

[25] Andrawes B, DesRoches R. Effect of ambient temperature on the hinge opening in bridges with shape memory alloy seismic restrainers. *Engineering structures.* 2007;29:2294 - 301.

[26] Araya R, Marivil M, Mir C, Moroni O, Sepulveda A. Temperature and grain size effects on the behavior of CuAlBe SMA wires under cyclic loading. *Materials science and engineering A - structural materials properties microstructure and processing.* 2008;496:209-13.

[27] British Standards Institution. BS 970-1:1996 - Specification for wrought steels for mechanical and allied engineering purposes. General inspection and testing procedures and specific requirements for carbon, carbon manganese, alloy and stainless steels: BSI; 1996.

[28] Torra V, Isalgue A, Lovey FC, Sade M. Shape memory alloys as an effective tool to damp oscillations Study of the fundamental parameters required to guarantee technological applications. *J Therm Anal Calorim.* 2015;119:1475-533.

[29] British Standards Institution. Bs En 12512:2001 - Timber structures - Test methods - Cyclic testing of joints made with mechanical fasteners: BSI; 2001.

[30] Miyazaki S, Imai T, Igo Y, Otsuka K. Effect of cyclic deformation on the pseudoelasticity characteristics of Ti-Ni alloys. *Metall Trans A.* 1986;17:115-20.